



Article

Enhance Formation of Hydroxyapatite and Corrosion Behavior Of Ti13Nb13Zr Alloy Coated with SiO₂, BaTiO₃ and SiO₂-BaTiO₃ Composite Comparative Study

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Abstract: Surface modification of titanium alloys is widely employed to improve their bioactivity and corrosion resistance for biomedical implant applications. In this study, Ti-13Nb-13Zr alloy samples were coated with SiO₂, BaTiO₃, and a SiO₂-BaTiO₃ composite using a spray pyrolysis technique. The coated specimens were immersed in simulated body fluid (SBF) for 30 days to evaluate their apatite-forming ability and bioactivity. The formation of hydroxyapatite and surface characteristics were investigated using X-ray diffraction (XRD), energy-dispersive X-ray spectroscopy (EDX), and field-emission scanning electron microscopy (FESEM). Electrochemical performance was assessed through open-circuit potential (OCP), potentiodynamic polarization, and electrochemical impedance spectroscopy (EIS). The results revealed successful hydroxyapatite formation on all coated surfaces, with the SiO₂-BaTiO₃ composite coating exhibiting the highest apatite-forming ability, as evidenced by increased hydroxyapatite peak intensity and a dense surface morphology. Electrochemical measurements demonstrated a significant improvement in corrosion resistance, with the composite-coated sample showing the lowest corrosion rate ($1.883 \times 10^{-5} \text{ mm} \cdot \text{y}^{-1}$), a protection efficiency of 99.49%, and the highest impedance resistance after SBF immersion. The enhanced performance was attributed to the synergistic effect of SiO₂ and BaTiO₃, which promoted hydroxyapatite deposition and improved surface protection. These findings suggest that SiO₂-BaTiO₃ composite coatings deposited by spray pyrolysis are a promising surface modification approach for improving the bioactivity and corrosion resistance of Ti-13Nb-13Zr alloy used in biomedical implants.

Keywords: Ti-13Nb-13Zr alloy; SiO₂-BaTiO₃ composite coating; Spray pyrolysis; Hydroxyapatite formation; Corrosion resistance; Simulated body fluid; Biomedical implants.

Citation: Al-Bayati S. M., Rustam H. K. Enhance Formation of Hydroxyapatite and Corrosion Behavior Of Ti13Nb13Zr Alloy Coated with SiO₂, BaTiO₃ and SiO₂-BaTiO₃ Composite Comparative Study. Central Asian Journal of Medical and Natural Science 2026, 7(3), 668-681.

Received: 10th Mar 2026

Revised: 11th Apr 2026

Accepted: 19th May 2026

Published: 23th Jun 2026



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Introduction

The hydroxyapatite (Ca₁₀(PO₄)₆(OH)₂) is an essential component of bone structure; together with collagen, they form the basis for bone formation and structure as shown in fig (1). Therefore, researchers have been studying how bone forms, especially in fluids similar to body fluids which they call simulated body fluid (SBF). Another studies have shown that the biomimetic formation of hydroxyapatite in the simulated body fluid is greatly affected by the surface on which it begins to form [1]. Titanium alloys were among the most commonly used alloys for manufacturing surgical implants especially Ti13Nb13Zr alloy. Numerous studies have addressed the coating of titanium alloys in

general with various bioceramic materials to accelerate bone growth. These bioceramics such as barium titanate BaTiO_3 and silicon dioxide SiO_2 have been the focus of these researches due to their role in accelerating bone growth [2]. Barium titanate (BaTiO_3) is a promising, lead-free piezoelectric ceramic heavily researched for advanced bone tissue engineering. It mimics the natural piezoelectricity of bone, enabling electrical microenvironments that actively promote cell growth, osteogenesis, and wound. Silicon dioxide (SiO_2), or silica, is highly versatile in biomedicine particularly in the form of bioglass. It is prized for its excellent biocompatibility, tunable pore size, large surface area, and ability to release silicate ions that promote bone regeneration [3]. For these characteristics our research we coat Ti13Nb13Zr alloy samples with SiO_2 , BaTiO_3 as individual and together as mix using pyrolysis spray coating and investigate how that coating affect the formation of hydroxyapatite after immersing in simulated body fluid for one month. XRD, EDX X, FESEM and electrochemical corrosion test was achieved to evaluate the results of these samples [4].

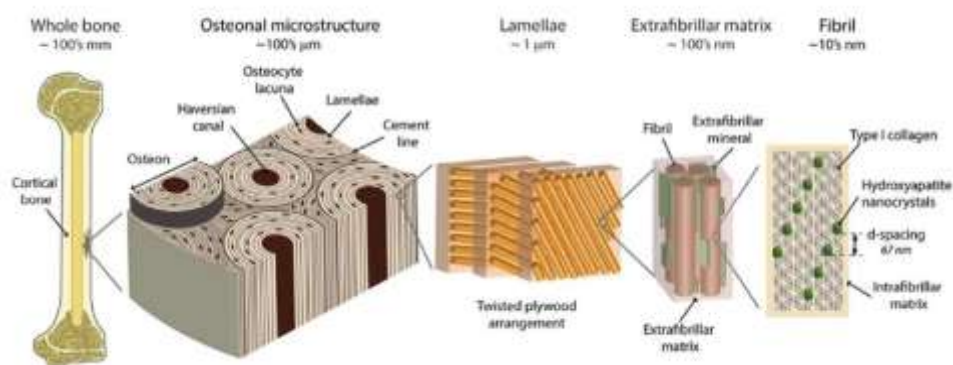


Figure 1. The hierarchical organization of cortical bone.

Materials and Methods

The samples were prepared by cutting Ti13Nb13Zr 20mm diameter rod with chemical composition listed in table (1) to 2mm thickness samples using wire cutting machine (DK-7735, China). The samples were grinded using grinding paper (p 120-400) grit and cleaned with acetone (Sigma Aldrich, USA) twice using ultrasonic cleaner bath (Camel FSF030s, China). The coating suspension was prepared by dissolving 1 gm from polyvinylpyrrolidone (PVP K30, CDH, India) in 10 ml water and stirred vigorously for 20 minutes using hot plate with magnetic stirrer (Alfa HS 860, Iran). Follow that step 40 ml of absolute ethanol was added and stirred gently for 10 minutes using hot plate with magnetic stirrer. Then 3 gm of SiO_2 (<30nm, Skyspring Nanomaterial, USA) was added to the previous solution and mixed gently for 10 minutes using hot plate with magnetic stirrer. In order to coating the samples we used spray gun connected to (5 psi pressure) air compressor with 0.1 mm diameter nozzle and spray the suspension from 10 cm distance after preheating the samples to 80 °C on hot plate as shown in fig (2). The coated procedure was repeated to achieve two coated layers, then the samples were heat treated at 100 °C for one hour under air atmosphere using oven (Silver cryst, Germany). Also second and third groups of Ti13Nb13Zr alloy 2 mm thickness samples was coated with BaTiO_3 (<40nm, Skyspring Nanomaterial, USA) and mixed composite from SiO_2 and BaTiO_3 with 50% of each one by using the same previous procedure of preparing composite solution and coating. The samples were immersed in synthetic simulated body fluid (SBF) for one month. The SBF solution was prepared by mixing the chemical component in table (1) in one liter of deionized water and mixed vigorously for 30 minutes using hot plate with magnetic stirrer. The pH of the SBF solution was adjusted to pH= 7.2 using pH meter (Hanna Instruments, HI2210, Germany) by adding diluted hydrochloric acid or diluted sodium hydroxide as required. The immersed samples were heat treated at 100°C in oven

for one hour under air atmosphere. The immersed samples were tested by XRD ,EDX and FESEM, then electrochemical corrosion test also achieved by testing OCP, polarization curve tafel, and electrochemical impedance spectroscopy EIS using potentiostat (CHI 604E, CHINA). The sample was connected as the working electrode, the graphite electrode as the counter electrode, and Ag/AgCl/KCl 3.5M electrode as the reference electrodes as shown in fig (3), while the corrosion media was (SBF) solution.

Table 1. chemical composition of Ti13Nb13Zr alloy.

Chemical composition [% wt.]							
Nb	Zr	Fe	C	H	O	S	Ti
13.18	13.49	0.085	0.035	0.004	0.078	<0.001	balanced

Table 2. chemical composition of simulated body fluid (SBF) solution.

ITEM	Reagent	Concentration g/l
1	8.035	NaCl
2	0.355	NaHCO ₃
3	0.225	KCl
4	0.231	K ₂ HPO ₄
5	0.311	MgCl ₂ .6H ₂ O
6	0.292	CaCl ₂
7	0.072	Na ₂ SO ₄

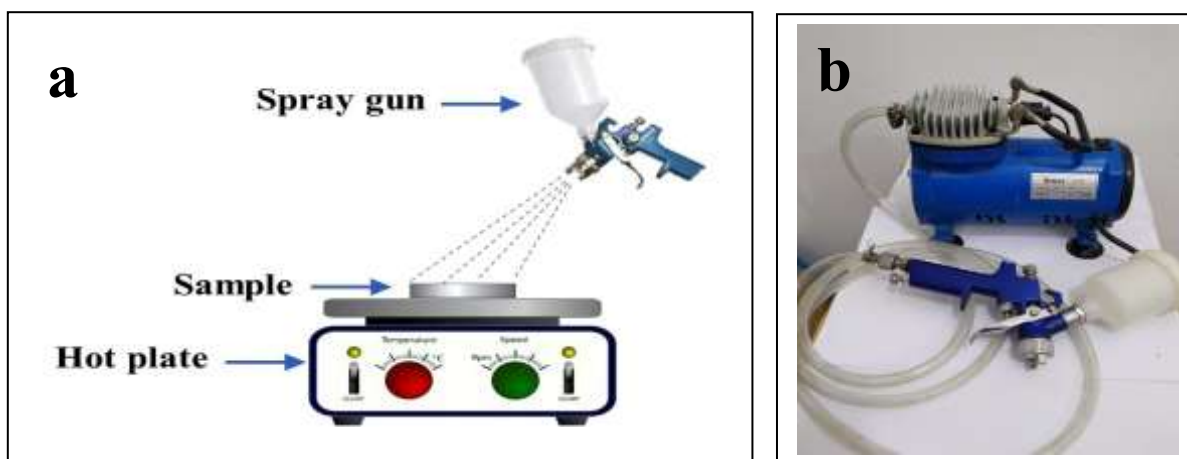


Figure 2. A: Simplified diagram for pyrolysis spray coating process, B: The pyrolysis spray system.

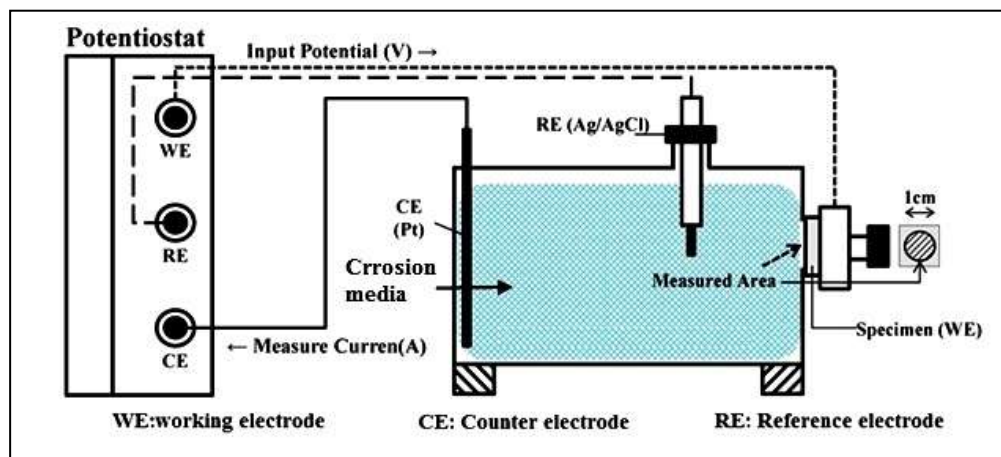


Figure 3. Schematic diagram for sample connection to the potentiostat for corrosion test.

Results

1-XRD Test:

The XRD pattern for Ti13Nb13Zr alloy uncoated sample in fig (4) shows the appearance of hydroxapatite peaks matching JCPDS standard card 00-009-0432 for hydroxyapatite after immersing in SBF solution and four peaks for titanium matching with JCPDS no. 00-044-1294 for titanium. The appearance of titanium peaks was an indicator for poor covering the sample surface with hydroxyapatite [5].

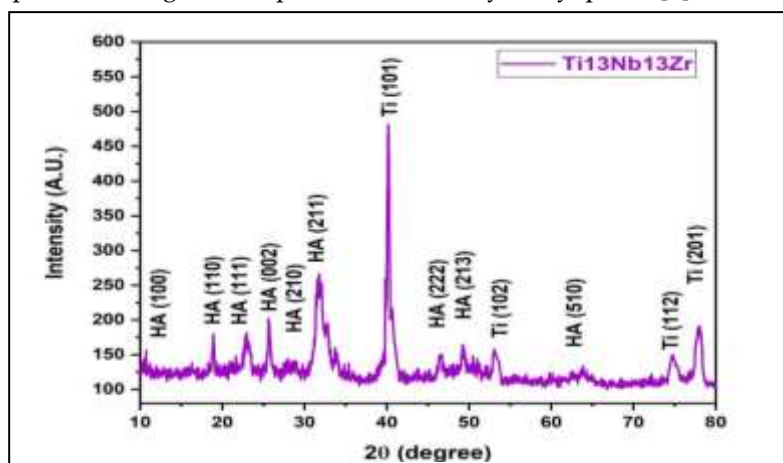


Figure 4. XRD pattern for Ti13Nb13Zr alloy uncoated sample.

The XRD pattern for sample coated with SiO₂ nanopowder in fig (5) shows obviously the appearance of hydroxapatite peaks matching JCPDS standard card 00-009-0432 for hydroxyapatite. Only one peaks appeared matching with JCPDS no. 00-040-1498 for SiO₂ and no titanium peak was observed in the pattern as indicator that the coating was covered the sample surface [6].

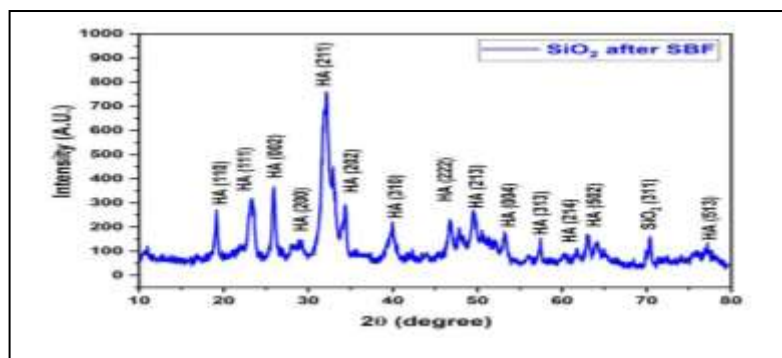


Figure 5. XRD pattern for SiO₂ after immersing in SBF solution for one month.

The XRD pattern for sample coated with BaTiO₃ nanopowder in fig (6) shows the appearance of hydroxyapatite peaks matching JCPDS standard card no. 00-009-0432 for hydroxyapatite and appearance of one peak for BaTiO₃ matching JCPDS standard card no.01-075-2116 for BaTiO₃ and also no titanium peak was observed in the pattern.

The XRD pattern for sample coated with SiO₂- BaTiO₃ mixture composite in fig (7) was also shows the hydroxyapatite peaks matching JCPDS standard card no. 00-009-0432 for hydroxyapatite and only one peaks appeared matching with JCPDS no. 00-040-1498 for SiO₂ and one peak observed for BaTiO₃ matching JCPDS standard card no.01-075-2116 for BaTiO₃. Also no titanium peak was observed in the pattern [7].

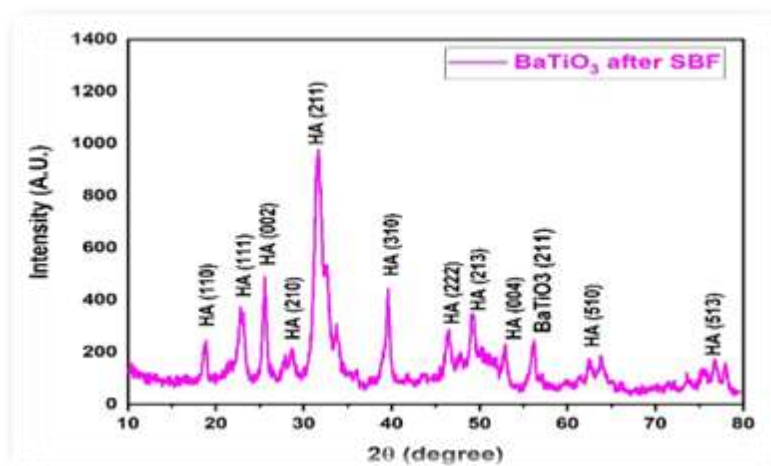


Figure 6. Fig (5) XRD pattern for BaTiO₃ after immersing in SBF solution for one month.

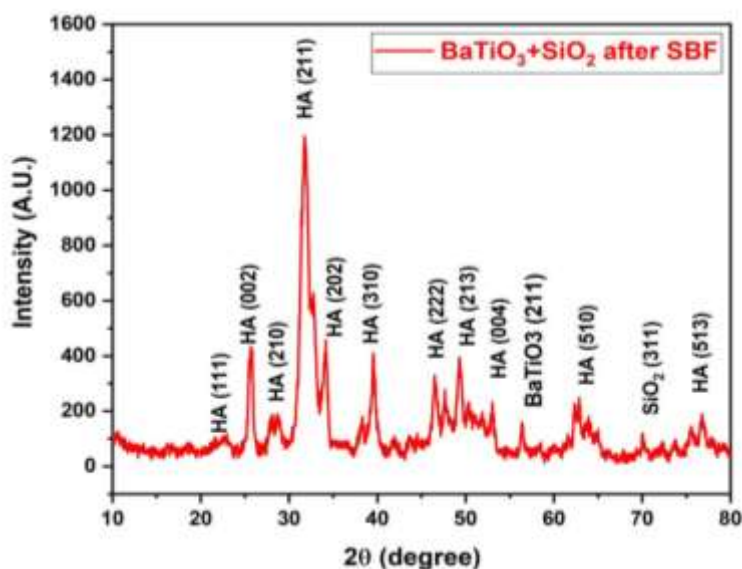


Figure 7. XRD pattern for SiO₂-BaTiO₃ mixture composite after immersing in SBF solution for one month.

Fig (8) shows the comparison for all coated samples. We see obviously the increasing in peaks intensity gradually from uncoated sample until that coated with SiO₂-BaTiO₃ mixture composite. Where that arrangement of increasing in intensity was uncoated base, SiO₂, BaTiO₃ and SiO₂-BaTiO₃ mixture composite. This indicate was the final sample was more biocompatible and has more ability to attract the hydroxyapatite and make it more grown over the sample surface, i.e. it has more osseointegration ability [8].

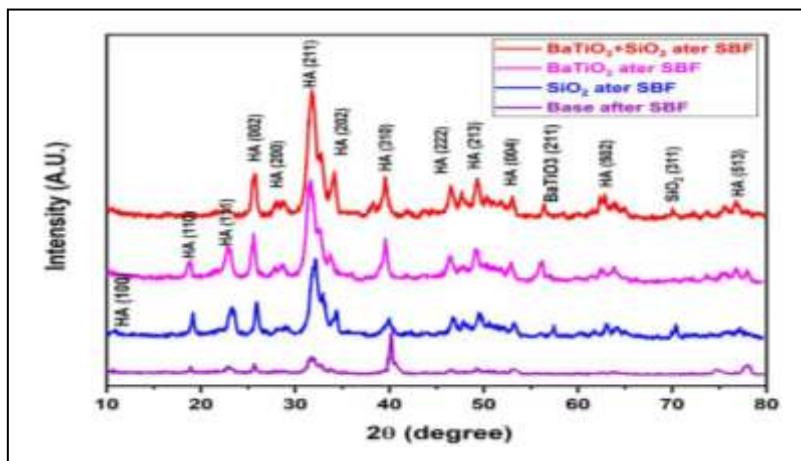


Figure 8. the XRD pattern comparison for all coated samples.

2-EDX test:

The EDX elemental analysis for uncoated alloy after immersing in SBF solution in fig (9) shows the appearance of calcium phosphorus and magnesium as indicator for hydroxyapatite formation. Also the appearance of titanium refers to high porous and uncovered sample surface with hydroxyapatite.

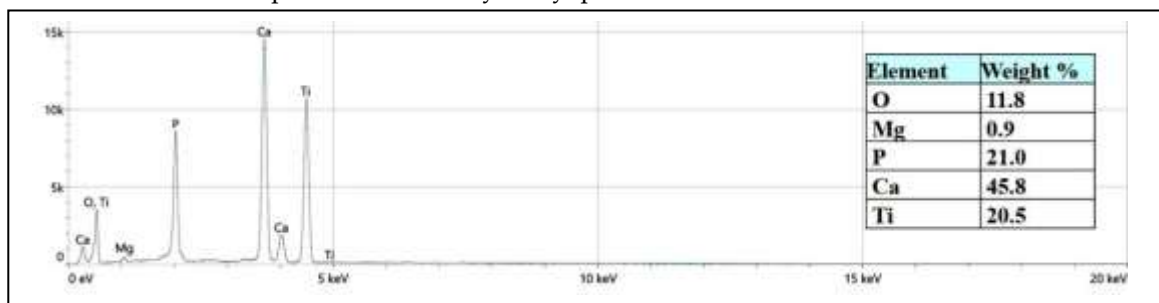


Figure 9. EDX elemental analysis for uncoated alloy after immersing in SBF solution.

The ratio of calcium to the phosphorus in natural hydroxyapatite ($\text{Ca}_{10}(\text{PO}_4)_6(\text{OH})_2$) known as 1.6667 as atomic ratio, so we can calculate it as weight percent ratio as below:

$$\text{Ca/P} = (10 \times \text{Ca Mwt.}) / (6 \times \text{P Mwt.})$$

Where Ca Mwt. = calcium molecular weight and P Mwt. = phosphorus molecular weight

$$(10 \times 40.078) / (6 \times 30.9737) = 2.1565$$

From EDX elemental analysis the Ca/P ratio for the hydroxyapatite formed from SBF solution was equal to 2.180 and it's very close to that for natural hydroxyapatite [9].

The EDX elemental analysis for sample coated with SiO_2 after immersing in SBF solution in fig (10) shows the appearance of calcium phosphorus, magnesium and sodium came from natural formation of hydroxyapatite. Also we see the appendence of silicone came from SiO_2 . There was no appearance of titanium or any element from base alloy, i.e. the covering of coating with SiO_2 and the natural formed hydroxyapatite cover the sample surface very well. The Ca/P ratio was 2.171 and it's also very close to that for natural hydroxyapatite [10].

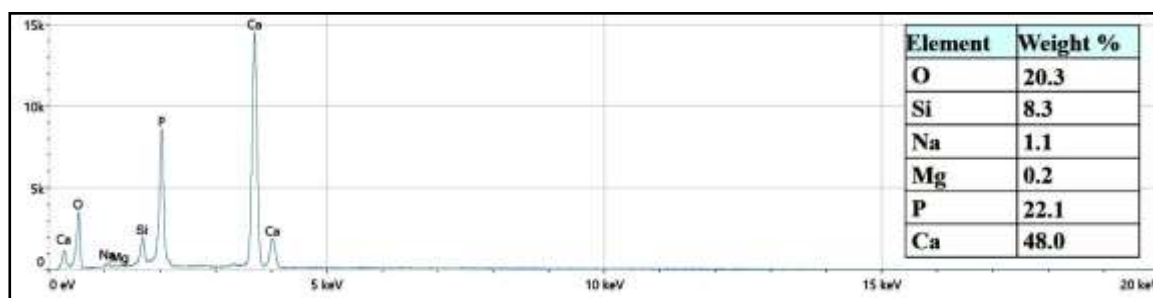


Figure 10. EDX elemental analysis for sample coated with SiO₂ after immersing in SBF solution.

The EDX elemental analysis for sample coated with BaTiO₃ after immersing in SBF solution in fig (11) shows the appearance of same elements as previous sample for same reason but with the appendence of barium and titanium came from BaTiO₃. The Ca/P ratio was 2.172 near to that for natural hydroxyapatite.

The EDX elemental analysis for sample coated with SiO₂ and BaTiO₃ mixture composite after immersing in SBF solution in fig (12) shows the appearance of the elements calcium phosphorus, magnesium and sodium came from hydroxyapatite formation beside silicone, barium and titanium came from SiO₂ and BaTiO₃ mixture. The Ca/P ratio was 2.182 near to that for natural hydroxyapatite.

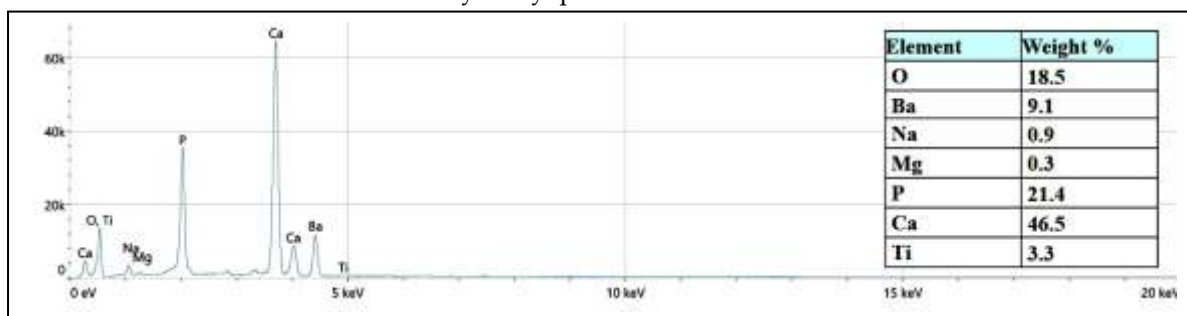


Figure 11. EDX elemental analysis for sample coated with BaTiO₃ after immersing in SBF solution.

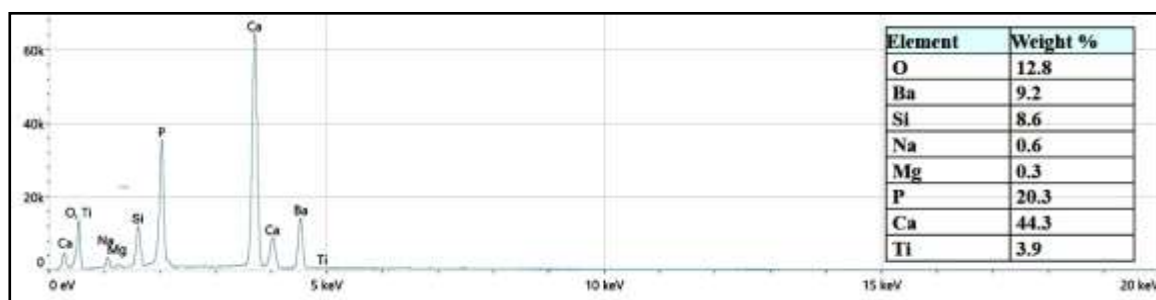


Figure 12. Fig (11) EDX elemental analysis for sample coated with SiO₂ and BaTiO₃ mixture after immersing in SBF solution.

3-FESEM test:

The FESEM test images for uncoated sample after immersing in SBF solution in fig (13 a and b) shows formation of hydroxyapatite on the sample surface where the shape of hydroxyapatite varied between agglomerated particles and flakes. The particle size varied between 62.49 to 98.72 nm.

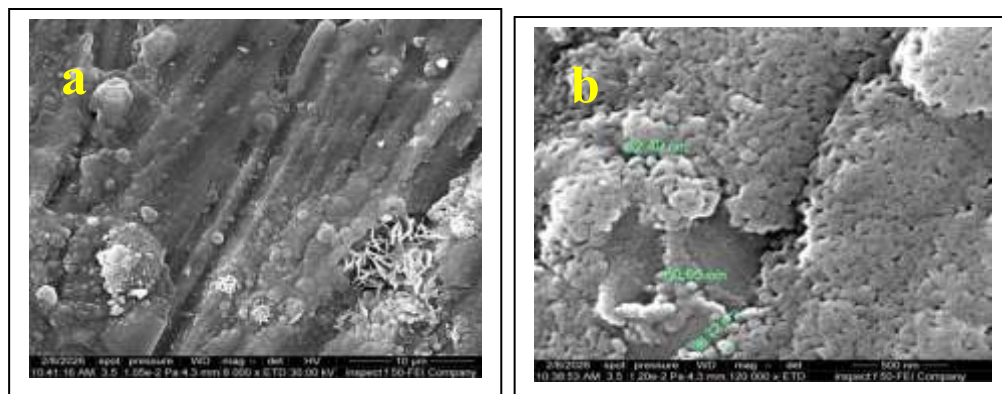


Figure 13. FESEM images for uncoated sample after immersing in SBF solution in different magnification [11].

Discussion

The FESEM images for samples coated with $\text{SiO}_2/\text{BaTiO}_3$ and $\text{SiO}_2\text{-BaTiO}_3$ mixture in fig (14 a-f) shows very thick porous layer of hydroxyapatite formed from SBF solution.

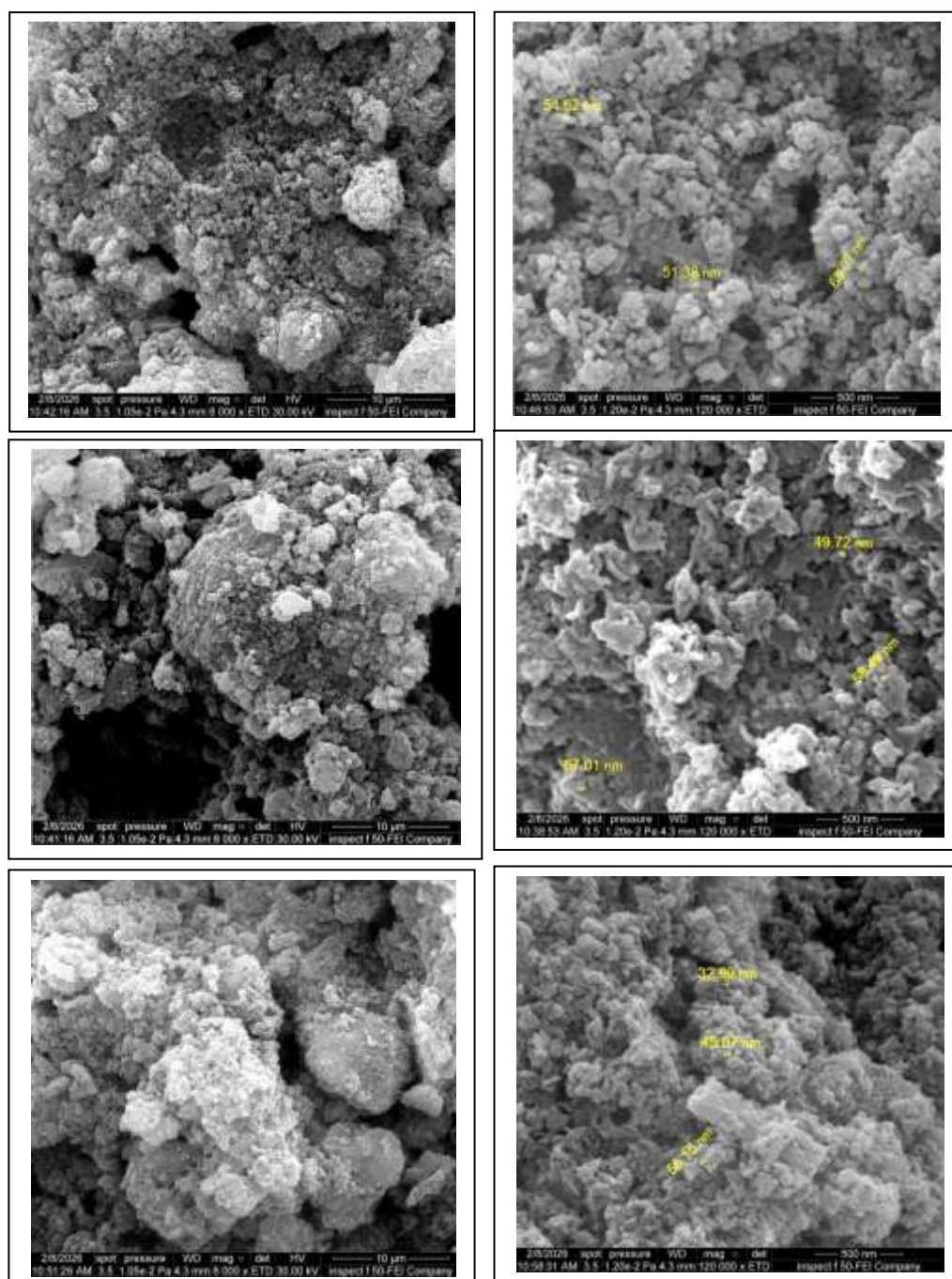


Figure 14. FESEM test images with different magnification for samples coated with (a ,b): SiO₂, (c,d): BaTiO₃, (E,F): SiO₂-BaTiO₃ mixture.

The FESEM test images for sample coated with SiO₂-BaTiO₃ mixture shows more agglomeration than that coated with BaTiO₃ and SiO₂ subsequently. The particle size for hydroxyapatite varied between 32.89 to 68.07 nm.

4- Electrochemical corrosion test:

Open circuit potential (OCP) TEST:

The OCP test shows gradually increasing in passivation from uncoated sample to that coated with SiO₂-BaTiO₃ mixture. Where the last one achieved 0.025 V compared with -0.655 for uncoated one before immersing [12].

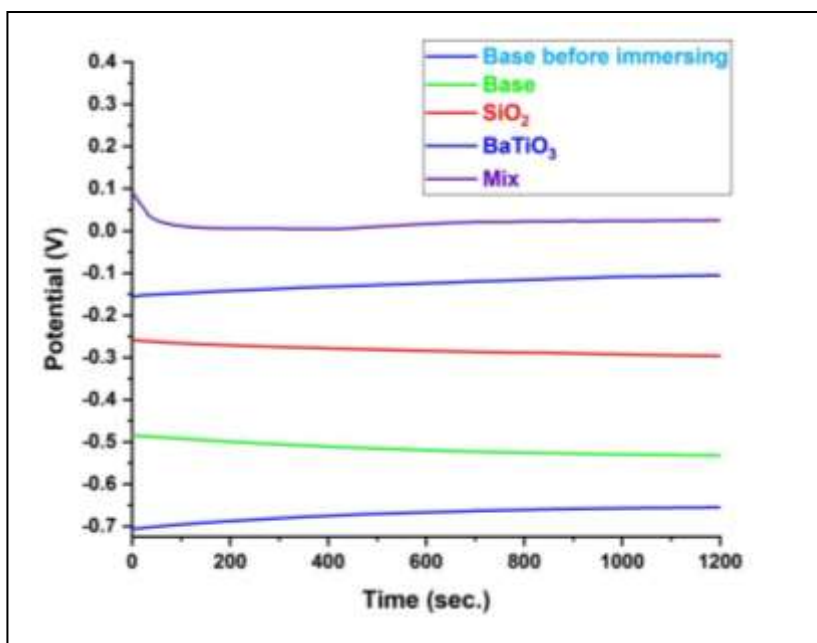


Figure 15. OCP test for all samples.

Table 3. OCP test results for all samples.

ITEM	OCP (volt)
Base before SBF	-0.655
Base	-0.531
SiO ₂	0.296-
BaTiO ₃	-0.105
MIX	0.025

Polarization curve (tafel) test:

The polarization curve comparison for all samples in fig (16) and table (4) shows decreasing in corrosion rate for sample coated with SiO₂-BaTiO₃ mixture more than the others, where it was achieve 1.883×10^{-5} mmpy compared with 3.716×10^{-3} mmpy for uncoated sample, i.e. the corrosion rate decreased about 197 times.

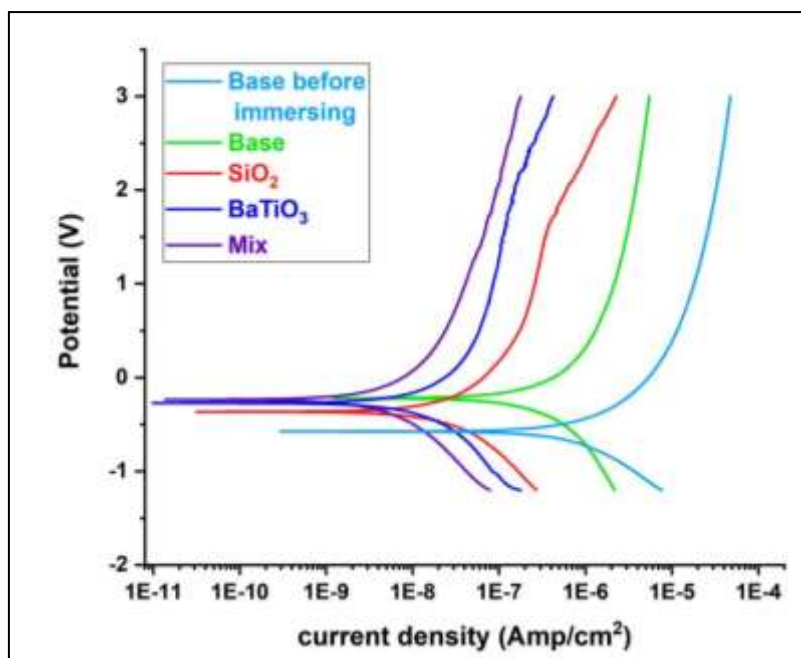


Figure 16. Polarization curve comparison for all samples.

Table 4. Parameters extracted from polarization curve (tafel) for all samples.

ITEM	Ecorr. (volt)	Icorr. (Amp)	Corr. Rate (mmpy)
Base before SBF	-0.556	4.224×10^{-7}	3.716×10^{-3}
Base	-0.219	8.590×10^{-8}	7.558×10^{-4}
SiO ₂	-0.364	8.450×10^{-9}	7.435×10^{-5}
BaTiO ₃	-0.258	4.212×10^{-9}	3.706×10^{-5}
MIX	-0.241	2.140×10^{-9}	1.883×10^{-5}

We can calculate the protection efficiency from the relation below:

$$PE\% = \frac{i_{corr. \text{ uncoated}} - i_{corr. \text{ coated}}}{i_{corr. \text{ uncoated}}} \times 100 \dots\dots$$

Where *i_{corr. uncoated}*: the corrosion current for uncoated sample after immersing in SBF and *i_{corr. coated}* the corrosion current for coated sample after immersing in SBF.

The calculated protection efficiency in table (5) shows that all samples except uncoated one achieved more than 97% protection efficiency, where the sample coated with SiO₂-BaTiO₃ mixture achieved the higher one equal to 99.49%.

Table 5. calculated protection efficiency for all samples.

ITEM	Icorr. (Amp)	protection efficiency %
Base before SBF	4.224×10^{-7}	-----
Base	8.590×10^{-8}	79.63
SiO ₂	8.450×10^{-9}	97.99
BaTiO ₃	4.212×10^{-9}	99.00
Mix	2.140×10^{-9}	99.49

Electrochemical impedance spectroscopy (EIS) test:

The EIS test was achieved for optimum sample (coated with SiO₂-BaTiO₃ mixture) compared with the un coated base before and after immersing in SBF solution. After fitting the resulting nyquist diagram for all samples we see that the uncoated sample shows a typical randles equivalent circuit before immersing in SBF solution as shown in fig (17 a and b). Also we see the coated sample shows an equivalent circuit for porous layer connected to the boundary double layer as shown in fig (18 a and b). After immersing in SBF solution the base sample shows different equivalent circuit for another porous layer formed on the sample surface shown in fig (19 a and b). Also the coated layer shows the formation of new porous layer connected to coated layer in the fitted equivalent circuit as

shown in fig (20 a and b). The comparison of all samples in fig (21) and table (6) shows how the new hydroxyapatite increase the resistance for both samples where the total resistance for uncoded sample increase to 10611 ohm compared with 2713 ohm before immersing, and the coated sample increased to 81348 ohm compared with 26346 ohm after immersing. This happened because the new hydroxyapatite formed layer filled the pores present in the previous SiO_2 and BaTiO_3 mixture layer and built another layer on top of it [13].

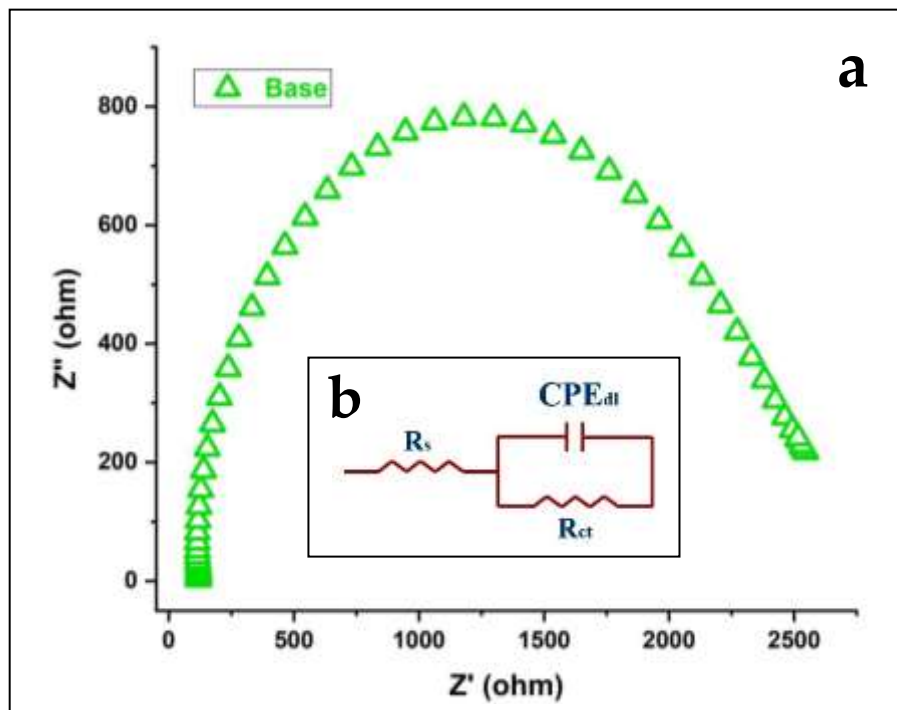


Figure 17. a: nyquist diagram for un coated base sample, b: equivalent circuit used for fitting.

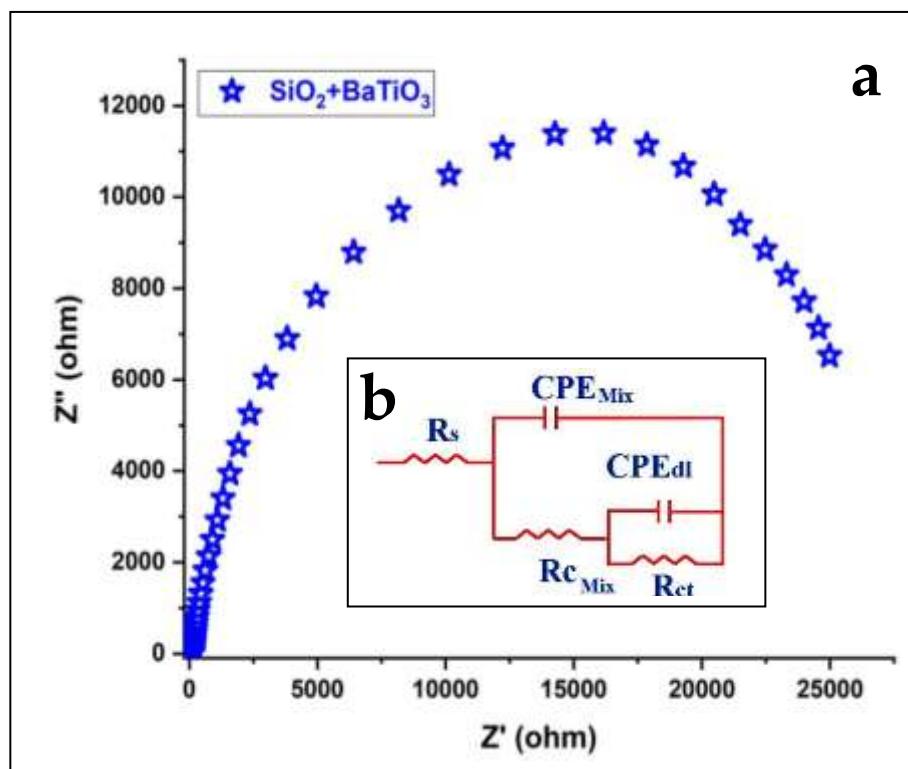


Figure 18. a: nyquist diagram for mixture coated sample, b: equivalent circuit used for fitting.

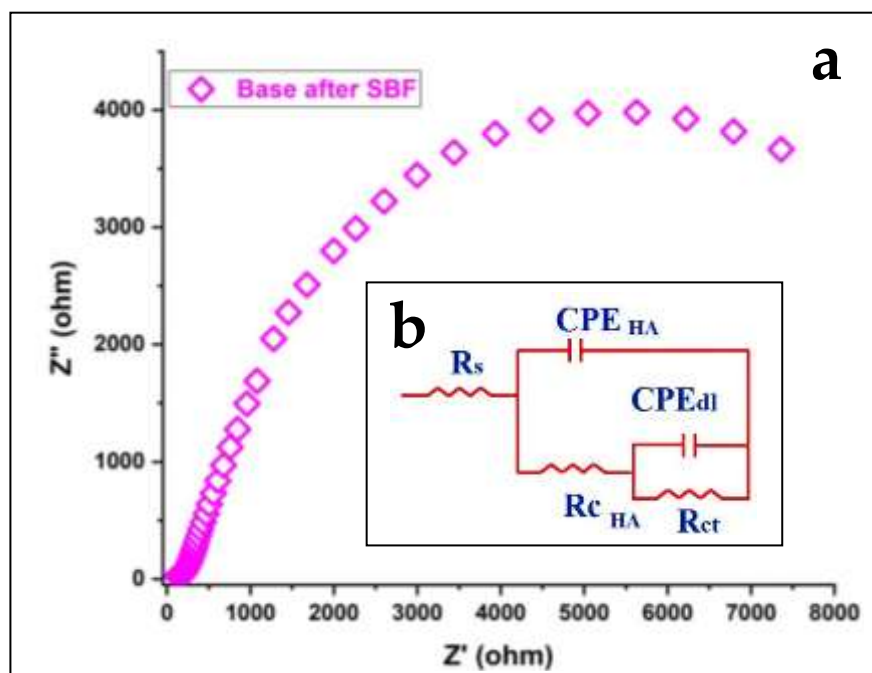


Figure 19. a: nyquist diagram for un coated base sample after immersing in SBF solution, b: equivalent circuit used for fitting.

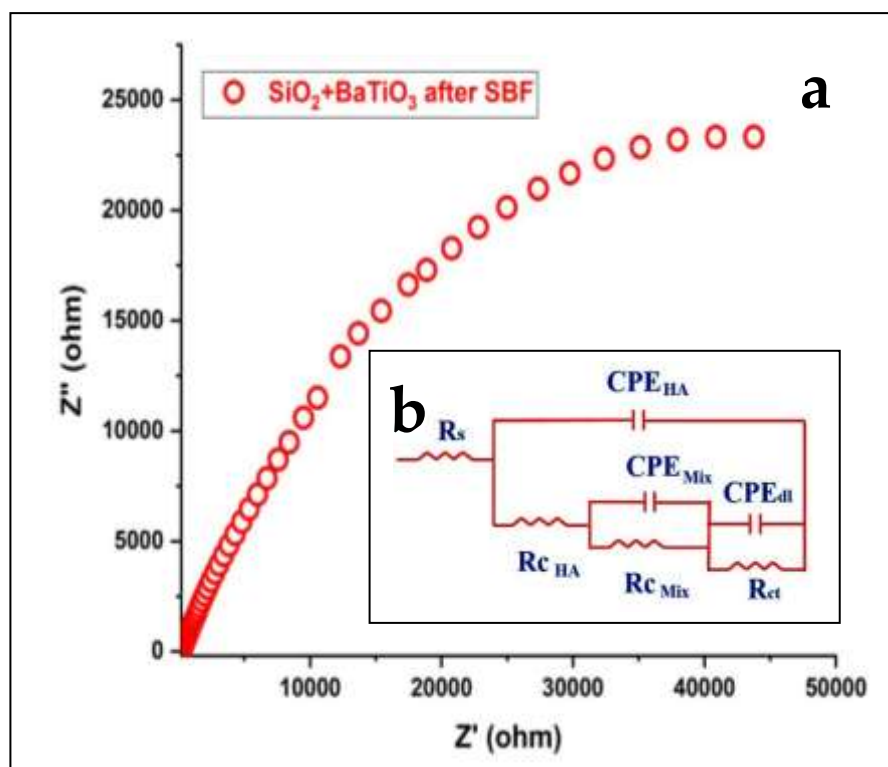


Figure 19. a: nyquist diagram for mixture coated sample after immersing in SBF solution, b: equivalent circuit used for fitting.

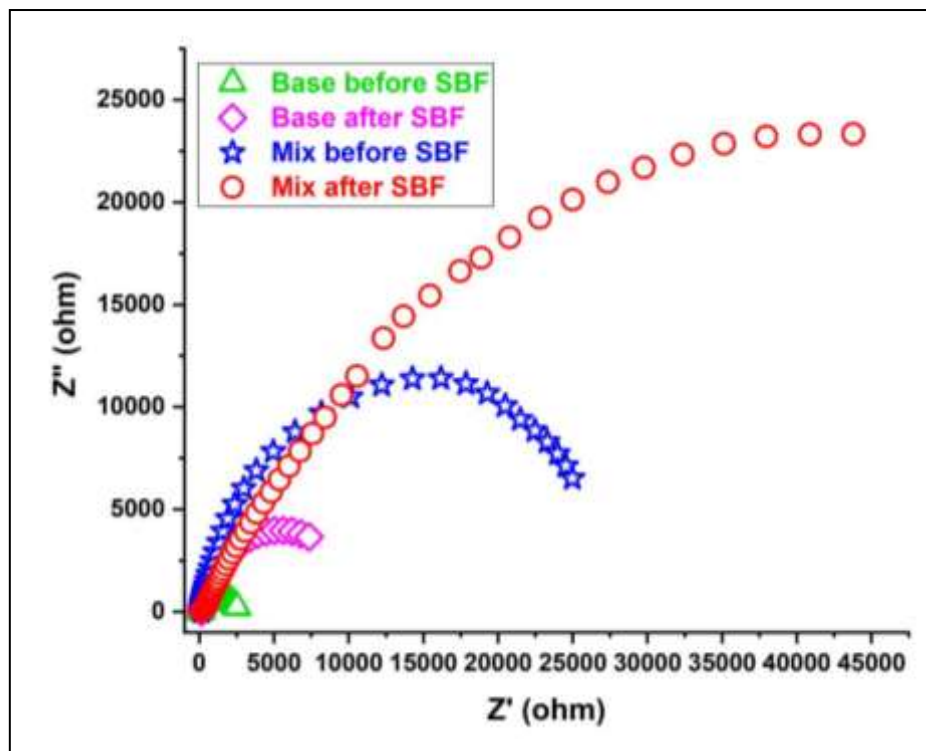


Figure 20. Nyquist diagram comparison for all samples.

Table 6. extracted parameters from fitting the two samples

Parameters	Before immersing in SBF		After immersing in SBF	
	Uncoated	Mix coated	Uncoated	Mix coated
R_s (ohm)	101	98	105	100
R_c (ohm)	----	23200	----	8631
R_{CHA} (ohm)	----	----	7430	68332
R_{dl} (ohm)	2612	3048	3079	4285
CPE_c (F)	----	3.7586E-04	----	1.5458E-06
n_1	----	0.997	----	0.919
CPE_{CHA} (F)	----	----	2.1418E-05	8.6654E-07
n_1	----	----	0.915	0.905
CPE_{dl} (F)	3.7221E-06	2.2116E-06	1.7508E-04	1.0002E-05
n_2	0.96469	0.939	0.994	0.921
R_{total} (ohm)	2713	26346	10614	81348

It is worth noting that the resistance of double layer also increased when hydroxyapatite formed on samples surface and fill the pores, where the for uncoated base sample increased from 2612 ohm to 3079 ohm, and for coated one increased from 3048 ohm to 4285 ohm [14]. This happened because when the hydroxyapatite filled the pores making it more difficult for the oxide layer to leave the sample surface and go to the corrosion media (SBF) so that it be an additional protected layer, the more difficult it becomes for the oxide layer to leave, the higher the resistance becomes, because the oxide continues to form and cannot leave the surface [15].

Conclusion

From previous results we conclude that the coating SiO_2 and $BaTiO_3$ mixture composite was best than coating with each biomaterial alone for the purpose of attracting hydroxyapatite from body fluid solutions and increasing bone formation. The XRD test proves the increasing in hydroxyapatite peaks intensity and FESEM test image shows more agglomeration when coating the sample with previous mixture. The corrosion test proves that the passivation will increase and corrosion rat will decreased about 197 times

than uncoated sample. The EIS test also prove the increasing in resistance after immersing in SBF solution and reach to 81348 ohm compared with 26346 ohm before immersing because theformation of hydroxyapatite which fill the pores of the coated layer and built another layer over it.

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